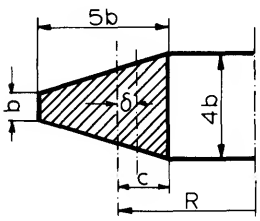
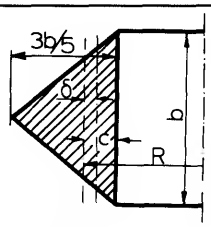
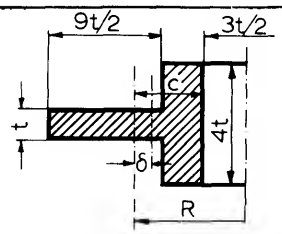
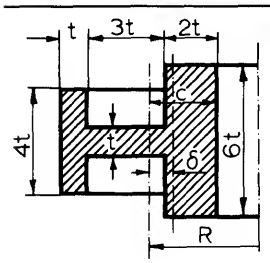
Table 28.2 (cont.)

	R/c	ϕ_o Inner Face	ϕ_o Outer Face	δ/R
	1.2	3.14	0.52	0.352
	1.4	2.29	0.54	0.243
	1.6	1.93	0.62	0.179
	1.8	1.74	0.65	0.138
	2.0	1.61	0.68	0.110
	3.0	1.34	0.76	0.050
	4.0	1.24	0.82	0.028
	6.0	1.15	0.87	0.012
	8.0	1.12	0.91	0.0060
	10.0	1.10	0.93	0.0039
	1.2	3.26	0.44	0.361
	1.4	2.39	0.50	0.251
	1.6	1.99	0.54	0.186
	1.8	1.78	0.57	0.144
	2.0	1.66	0.60	0.116
	3.0	1.37	0.70	0.052
	4.0	1.27	0.75	0.029
	6.0	1.16	0.82	0.013
	8.0	1.12	0.86	0.0060
	10.0	1.09	0.88	0.0039
	1.2	3.63	0.58	0.418
	1.4	2.54	0.63	0.299
	1.6	2.14	0.67	0.229
	1.8	1.89	0.70	0.183
	2.0	1.73	0.72	0.149
	3.0	1.41	0.79	0.069
	4.0	1.29	0.83	0.040
	6.0	1.18	0.88	0.018
	8.0	1.13	0.91	0.010
	10.0	1.10	0.92	0.0065
	1.2	3.55	0.67	0.409
	1.4	2.48	0.72	0.292
	1.6	2.07	0.76	0.224
	1.8	1.83	0.78	0.178
	2.0	1.69	0.80	0.144
	3.0	1.38	0.86	0.067
	4.0	1.26	0.89	0.038
	6.0	1.15	0.92	0.018
	8.0	1.10	0.94	0.010
	10.0	1.08	0.95	0.0065

the relevant values for the inner surfaces of the beams, where the critical stresses are usually found, a wide range of the factors may be represented by a single design curve such as that shown in Fig. 28.2. Since according to the customary procedure in curved-beam and hook design generous factors of safety are recommended, ball-park estimates such as those based on Fig. 28.2 may be acceptable [161] during the preliminary stages of hardware sizing. This approximation increases in accuracy as the cross sections of the curved members become more compact and have fewer abrupt changes of contour.